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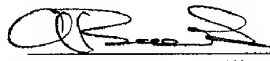
Date December 3, 1999

Docket No. 3045-2339

CERTIFICATION UNDER 37 CFR 1.10

I hereby certify that this New Application Transmittal and the documents referred to as enclosed therein are being deposited with the United States Postal Service on this 3rd day of December, 1999 in an envelope as "Express Mail Post Office to Addressee" Mailing Label Number EL398955921US addressed to: Box Patent Application, Assistant Commissioner of Patents, Washington, D.C. 20231.

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Washington, D.C. 20231

NEW APPLICATION TRANSMITTAL

Transmitted herewith for filing is the patent application of

Inventor(s): SUZUKI, Yuzuru; FUJITANI, Sakae; KAGAWA, Masaki

For : Actuator

Enclosed are:

1. Benefit of Prior U.S. Application (35 USC)

_____ The new application being transmitted claims the benefit of a _____ and enclosed is added page for new application transmittal where benefit of a prior U.S. application claimed.

2. The Papers Required For Filing Under 37 CFR 1.53:

<u>25</u>	Pages of Specification
<u>1</u>	Pages of Abstract
<u>3</u>	Pages of Claims
<u>7</u>	Sheets of Drawing

 X formal informal

In addition to the above papers there is also attached:

<u> </u>	Pages of an Amendment
<u> x </u>	Return Receipt Postcard
<u> </u>	Information Disclosure Statement with <u> </u> copies of references.

3. Declaration or oath

☒ Enclosed 3 pages
☒ Newly executed (original or copy)
☐ Copy from a prior application (continuation/divisional with page 5 of 5 completed)
☐ Deletion of Inventor(s) (signed statement attached deleting inventor(s) of prior application)
☐ Not enclosed

4. Inventorship Statement

The inventorship for all the claims in this application are:

☒ the same

OR

☐ are not the same and an explanation, including the ownership of the various claims at the time the last claimed invention was made, is submitted.

5. Language

☒ English ☐ Non-English

A verified English translation of the

[check applicable item(s)]

☐ specification and claims

☐ declaration

is attached.

6. Assignment

☒ An assignment of the invention to Minebea Co., Ltd.

☒ is filed under separate cover sheet

☐ was filed in the prior application

☐ will follow

7. Certified Copy

Japan

(Country)

344528/1998

(Application No.)

December 3, 1998

(Filed)

from which priority is claimed

☒ is attached

☐ will follow

8. Fee Calculation

CLAIMS AS FILED

	Number Filed	Provided with Basic Fee	Number Extra	Rate	Basic Fee \$760
Total Claims	10	20	0	X \$18.00	\$.00
Independent Claims	1	3	0	X \$78.00	\$.00
Multiple Dependent Claim(s), if any	0	0	0	X \$260.00	\$.00

☐ Amendment canceling extra claims enclosed

☐ Amendment deleting multiple dependencies enclosed

☐ Fee for extra claims is not being paid at this time

Filing Fee Calculation \$ 760.00

9. Small Entity Statement

☐ verified statement that this is a filing by a small entity under 37 CFR 1.9 and 1.27 is attached.

Filing Fee Calculation (50% of above) \$ _____

10. Fee Payment Being Made At This Time

☒ Enclosed

☒ basic filing fee \$ 760.00

Total fees enclosed \$ 760.00

11. Method of Payment of Fees

☒ check in the amount of \$ 760.00

12. Authorization to Charge Additional Fees

☒ The Commissioner is hereby authorized to charge the following additional fees which may be required to Account No. 18-1829;

☒ 37 CFR 1.16 (filing fees and presentation of extra claims)

☒ 37 CFR 1.17 (application processing fees)

☐ 37 CFR 1.18 (issue fee at or before Mailing of Notice of Allowance, pursuant to 37 CFR 1.311(b)).

14. Correspondence Address

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ACTUATOR

BACKGROUND OF THE INVENTION

5 1. Field of the Invention

The present invention relates to a structure of a single-phase, claw pole type actuator and, more particularly, to a small, high-efficiency actuator that permits easy assembly and features a large detent torque and stable rotational repetitive operation.

10 2. Description of the Related Art

A so-called toroidal actuator with a toroidal winding wrapped around an annular core is known as an actuator for controlling angles by performing rotational repetitive operation. The toroidal actuator scarcely has a cogging torque and allows angle control to be achieved with good controllability and responsivity. The cogging torque is a torque produced when a coil is in a deenergization mode and hereinafter is referred to as "detent torque".

20 The toroidal actuator, however, has various problems in that the toroidal winding is difficult to wind and has so small detent torque that energizing current must be kept flowing or a spring or the like must be used to forcibly urge the actuator at all times in an initial state wherein no energization is performed in an application wherein a given direction of operation must be always maintained.

For this purpose, there is also a cross-coil

actuator that has a D-shaped soft magnetic material which forms a magnetic circuit and which covers an entire outer periphery of a single-phase winding unit so as to impart a detent torque. This type of actuator, however, is

5 disadvantageous in that it exhibits poor magnetic circuit efficiency and inevitably becomes large and also poses a problem in that an external shape thereof cannot be circular.

Thus, there have been demands for a small,

10 inexpensive actuator designed to have such functions and characteristics as operation of maintaining a rotor in a given direction by an appropriate detent torque in an initial state, and of performing a given operation for a period of time that corresponds to a time of energization

15 of a coil, and of inversely energizing the coil to forcibly set it back to the initial state, although the actuator is not required to conduct accurate angle control by a closed loop.

20 SUMMARY OF THE INVENTION

The present invention has been made with a view to solving the problems described above, and an object thereof is to provide an inexpensive, small, high-efficiency actuator that has a single-phase claw pole structure,

25 features easy assembly or winding, and is capable of activating a rotor in a certain given direction by a detent torque in a deenergization mode.

To this end, according to a first aspect of the present invention, there is provided a claw pole type actuator of a single-phase structure, comprising: a stator yoke composed of a pair of substantially circular planar yokes formed of a soft magnetic material, polar teeth which axially protrude from inner peripheral edges of the respective planar yokes and which are disposed to face each other, extending in an axial direction, and a cylindrical ring provided on outer peripheral edges of one of the planar yokes; an armature being constituted by installing a coil formed by winding a magnet wire in a coil receiving section shaped like an annular recess formed by the planar yokes, the polar teeth, and the cylindrical ring of the stator yoke; and a stator assembly which has flanges with bearings provided on both end surfaces of the armature and in which a rotor provided with a magnet for a magnetic field composed of a permanent magnet being installed to face the polar teeth of the stator with minute gaps provided therebetween; wherein a number of the polar teeth equals a number N of rotor magnetic poles (N is 2 or 4).

In a preferred form of the invention, the stator yoke is comprised of a first stator yoke in which a planar yoke and a polar tooth are combined into one piece, and a second stator yoke in which a planar yoke, polar teeth, and a cylindrical ring are combined into one piece, and the polar teeth in the first and second stator yokes are provide with the spacing of about respectively, are

disposed at an interval of approximately 180 degrees in terms of an electrical angle.

In another preferred form of the invention, a pair of stator yokes, each being composed of the planar yoke and the cylindrical ring combined into one piece, are disposed to face each other.

In yet another preferred form of the invention, the rotation of the rotor is restricted by a stopper so that a maximum angle of the rotational motion stays within a range of $120/N$ to $240/N$ degrees (N is 2 or 4).

Preferably, the stopper is incorporated in the actuator.

In a further preferred form of the invention, a groove or a cut for destroying magnetic balance is provided on a central portion of one of the south pole and the north pole of the magnet for magnetic field.

In a further preferred form of the invention, the extensions of the two polar teeth in a circumferential direction are all the same and stay within a range of $220/N$ to $260/N$ degrees (N is 2 or 4) in terms of central angle.

In a further preferred form of the invention, air gaps in a radial direction formed by the polar teeth and the rotor magnet are uneven, and air gaps at central portions of the polar teeth are narrower than air gaps at ends of the polar teeth.

Preferably, the flange is composed of a nonmagnetic material.

In a further preferred form of the invention, a relationship between a detent torque T_d (Nm) and a rated torque T_{rate} (Nm) is as follows:

$$T_{rate}/4 \leq T_d \leq 3 T_{rate}/4$$

5 where T_{rate} denotes a maximum torque value obtained when a rated current is caused to flow, and detent torque T_d denotes a maximum torque when a coil is in a deenergization mode.

10 BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is an exploded perspective view of an actuator according to a first embodiment of the present invention.

Fig. 2A is a schematic representation illustrating a principle of operation of an actuator in conjunction with unifiler winding and bipolar drive, and Fig. 2B is a schematic representation illustrating in conjunction with bifiler winding and unipolar drive.

Fig. 3 shows a torque characteristic of the actuator in accordance with the present invention.

Fig. 4 shows a torque characteristic of the actuator in accordance with the present invention.

Fig. 5 shows a torque characteristic of the actuator in accordance with the present invention.

25 Fig. 6 is a perspective view showing a second embodiment of the present invention.

Fig. 7 is a perspective view showing a third

embodiment of the present invention.

Fig. 8A is a perspective view showing a bearing of a fifth embodiment of the present invention, and Fig. 8B is a perspective view showing a rotor of the fifth embodiment.

5 Fig. 9 is a perspective view showing a sixth embodiment of the present invention.

Fig. 10 is a sectional view showing a fourth embodiment of the present invention.

10 Fig. 11 is a sectional view showing a seventh embodiment of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Embodiments of an actuator having a single-phase claw pole structure in accordance with the present
15 invention will now be described.

Fig. 1 is an exploded perspective view of an actuator according to a first embodiment of the present invention.

In the embodiment, a stator yoke is comprised of a
20 first stator yoke 2 formed of a planar yoke section and a polar teeth section that are combined into one piece, and a second stator yoke 4 formed of a planar yoke section, a polar teeth section and a cylindrical ring section that are combined into one piece. The rotor of this embodiment has
25 two magnetic poles by way of example.

An actuator 10 is constituted by four sections, namely, a rotor 1, an armature 9, upon and lower flanges 6

and 7 and bearings 5. The armature 9 is constituted by three sections, namely, a first stator yoke 2, a coil assembly 3, and a second stator yoke 4. The upper flange 6 is provided with mounting holes 20 for coupling to an external unit.

First, the rotor 1 is fixed by concentrically securing a magnet 30, which is magnetized to have two poles, to a rotary shaft 21 via a sleeve 22. In this embodiment, the magnet 30, the sleeve 22, and the rotary shaft 21 are fixed by adhesives.

The armature 9 is composed of the first stator yoke 2, the coil assembly 3, and the second stator yoke 4. The first stator yoke 2 is formed of a substantially toroidal planar yoke 23 and a polar tooth 25 that projects in an axial direction from an inner peripheral edge of the yoke 23 and extends in a circumferential direction, the yoke 23 and the polar tooth 25 being integrally formed. To be more specific, in this embodiment, the polar tooth is formed by vertically punching and raising a central portion of a disc-shaped soft magnetic steel plate (a pure iron or a galvanized steel plate) in an axial direction. The planar yoke 23 shown in Fig. 1 is provided with a positioning projection 24 for establishing a circumferential positional relationship with respect to the second stator yoke 4, which will be explained hereinafter.

The coil assembly 3 is formed by winding a coil 28 around a resinous bobbin 29 (which may be for example, a

liquid crystal polymer). In this embodiment, a terminal block 26 in which terminals 27 have been inserted is integrally resin-formed with a jaw of the bobbin 29. The terminal block 26 is designed to be fitted in a notch 33
 5 formed on the upper edge of a cylindrical ring 31 of the second stator yoke 4, which will be discussed hereinafter.

The second stator yoke 4 is similar to the first stator yoke 2 in that the substantially disc-shaped planar yoke 23 is made integral with the polar tooth 25 that
 10 axially protrudes from an inner peripheral edge of the yoke 23 and extends in a circumferential direction, whereas the second stator yoke 4 differs from the first stator yoke 2 in that it is further provided with a cylindrical ring 31 which is integrally added to an outer peripheral edge of
 15 the planar yoke 23 in an axial direction by deep drawing such that it is parallel to the polar tooth 25. As previously mentioned, the cylindrical ring 31 of the second stator yoke 4 is provided with the notch 33 for performing circumferential positioning so that the polar tooth 25 of
 20 the first stator yoke 2 and the polar tooth 25 of the second stator yoke 4 have a phase difference of about 180 degrees in terms of an electrical angle. The terminal block 26 of the coil assembly 3 can be fitted in the notch 33.

25 The rotor 1 is arranged inside the actuator 9, and the bearings 5 are installed in central holes 32 of the upper and lower flanges 6 and 7, respectively, so that the

rotor 1 is rotatably supported by the bearings 5. A spacer 8 is arranged for axial positioning of the magnet 30 of the rotor 1 and the polar teeth 25 and for adjusting an axial play. The upper and lower flanges 6 and 7 and the bearings 5 are fixed by adhesives, and the flanges 6 and 7 are fixed to the first and second stator yokes 2 and 4 by adhesives in this embodiment; however, they may be alternatively fixed by mechanical caulking, welding, resin integral molding, etc. Further alternatively, the flanges may be made by resin molding.

The principle of operation and torque characteristics of the actuator with the single-phase claw pole structure in accordance with the present invention will now be described.

Fig. 2A is a schematic representation illustrating a principle of operation of the actuator in accordance with the present invention in conjunction with unifiler winding and bipolar drive, and Fig. 2B is a schematic representation illustrating the principle of operation of the actuator in conjunction with the bifiler winding and unipolar drive.

The principle of operation of the unifiler winding combined with the bipolar drive illustrated in Fig. 2A and that of the bifiler winding combined with the unipolar drive illustrated in Fig. 2B are similar; hence, descriptions will be given by reference to Fig. 2A.

Fig. 2A shows the coil 28 that represents a stator

section and the magnet 30 for magnetic field (hereinafter referred to simply as "the magnet 30") that represents a rotor section. The coil 28 has two modes, namely, one mode for passing a current I_1 from terminal A in a direction indicated by an arrow, and another mode for passing a current I_2 from terminal B in a direction indicated by the arrow. First, when the coil 28 is energized in the direction of I_1 , then terminal B, which is near the magnet 30, will be energized to be the north pole. This causes the south pole end of the magnet 30 to be attracted to terminal B of the coil. As a result, a torque in a direction indicated by a clockwise (CW) arrow acts, and the magnet 30 stops with the south pole thereof facing terminal B of the coil 28, that is, the magnet rotates 90 degrees clockwise from a state of the magnet 30 shown in Figs. 2A and 2B.

Conversely, if the coil 28 is energized in the direction of I_2 , then terminal B, which is near the magnet 30, is energized to be the south pole. This causes the north pole end of the magnet 30 to be attracted to terminal B of the coil 28. As a result, a torque in a direction indicated by a counterclockwise (CCW) arrow acts, and the magnet 30 stops with the north pole thereof facing terminal B of the coil 28, that is, the magnet 30 rotates 90 degrees counterclockwise from a state of the magnet 30 shown in Figs. 2A and 2B. Thus, in principle, if nothing restricts the rotation of the magnet 30, the actuator performs the

180-degree (± 90 degrees) repetitive rotational motion by energization.

Fig. 3, Fig. 4, and Fig. 5 respectively show torque characteristics of the actuator in accordance with the present invention.

Since the actuator in accordance with the present invention has the claw pole structure, it has a detent torque in a deenergization mode. Therefore, if a friction torque is ignored, a resultant torque equals a sum of the detent torque and an energizing torque. In the present invention, a torque generated when the coil is energized at a rated current will be referred to as a "rated torque," and a maximum value thereof will be denoted as T_{rate} . The relationships among these torques are shown in Figs. 3, 4, and 5, among which Figs. 3 and 4 illustrate typical torque characteristics of the first embodiment in which the detent torque (approximated to a sinusoidal wave, and the maximum value is denoted as T_d) is half as much as a rated torque (approximated to a sinusoidal wave, and the maximum value is denoted as T_{rate}), i.e. $T_d = T_{rate}/2$.

In Figs. 3, 4, and 5, relative angle differences θ (represented in terms of angles (degrees) between the rotor and the stator) are shown on the axis of abscissa, and torque values (represented as "torque") associated with the relative angle differences θ are shown on the axis of ordinates. For the convenience of explanation, positive torque is defined as torque in the direction indicated by

the clockwise arrow, while negative torque is defined as torque in the direction indicated by the counterclockwise arrow to associate them to the rotational directions of the rotor shown in Figs. 2A and 2B. In Figs. 3 and 4, solid

5 lines A denote curves of resultant torques (current passes in the direction indicated by arrow I_1 in Figs. 2A and 2B), dashed lines B denote curves of rated torques (the current passes also in the direction indicated by arrow I_1), and one-dot chain lines C denote curves of detent torques. Fig.

10 4 also shows a case wherein current passes in the direction indicated by arrow I_2 in addition to the case shown in Fig. 3. Referring to Fig. 3, if an angle θ ranges from 0 to 180 degrees (or from 180 to 360 degrees), then the resultant torque produced by current I_1 will be positive (or

15 negative), and a torque in the clockwise (or counterclockwise) direction is generated, causing the magnet to rotate clockwise (or counterclockwise) and stop at a position where torque is zero, i.e. $\theta = 180$ ($\theta = 180$) degrees. Referring now to Fig. 4, if an angle θ ranges

20 from 0 to 180 degrees (or from 180 to 360 degrees), then the resultant torque produced by current I_2 will be negative (or positive), and a torque in the counterclockwise (or clockwise) direction is generated, causing the magnet to rotate counterclockwise (or

25 clockwise) and stop at a position where torque is zero, i.e. $\theta = 0$ ($\theta = 360 = 0$) degree. This coincides with the explanation given in conjunction with Figs. 2A and 2B.

Descriptions will now be given of a relationship among detent torque, a repetitive rotational motion range, and a stopper, which is an important characteristic of the present invention.

5 This type of actuator is characterized in that detent torque T_d is large in relation to rated torque T_{rate} ; hence, a unique operation is possible by making use of the detent torque, which will be discussed in detail later. On the other hand, the detent torque causes a curve
10 of the resultant torque to be distorted as compared with a waveform of rated torque alone.

Fig. 5 shows a torque curve observed when detent torque T_d is relatively large in comparison with rated torque T_{rate} . More specifically, Fig. 5 shows a case
15 wherein $T_d = 0.8 T_{rate}$. As is obvious from Fig. 5, the curves of Fig. 5 are different from those of Figs. 3 and 4 in that the curves of the resultant torques are distorted more. In addition, although the angles stay within the range of 0 to 180 degrees (or 180 to 360 degrees), the
20 resultant torques turn to negative (or positive) in the range of 0 to θ_5 (or 180 to θ_7) degrees and the range of θ_4 to 180 (θ_6 to 360) degrees. This means that the actuator does not carry out the repetitive rotational motion unless the angles are within a range that is narrower than the
25 range of θ_4 to θ_5 . The reason is that the signs of all detent torque, resultant torque (in the I_1 direction), and the resultant torque (in the I_2 direction) agree with each

other in the ranges of 0 to θ_5 (or 180 to θ_7) and θ_4 to 180 (θ_6 to 360) degrees, so that the rotor cannot be rotated against the detent torque regardless of a direction in which current is passed. Thus, in the present invention,
5 relatively large detent torque T_d tends to narrow the range of the repetitive rotational motion.

Referring back to Fig. 4, the relationship among the detent torque, the repetitive rotational motion range and the stopper will be described.

10 In Fig. 4, if it is assumed that an actuator has stopper 1 and stopper 2 at positions of θ_1 and θ_2 , respectively, and the rotor is set so that it can perform repetitive motion only in a range from θ_1 to θ_2 , then the actuator will perform a series of operations described
15 below.

If the rotor lies between θ_3 and θ_1 (θ_2 and θ_3) when the coil is in the deenergization mode, then the detent torque is positive (or negative); hence, the rotor is rotated by a torque in the clockwise (or counterclockwise)
20 direction and stopped at the position of θ_1 (or θ_2) of the stopper 1 (or the stopper 2) and held at the position. In this state, if current is continued to be passed in an I_2 (or I_1) direction, then the rotor overcomes a positive detent torque and generates a torque in the
25 counterclockwise (or clockwise) direction and stops at the position of θ_2 (or θ_1) of the stopper 2. It is needless to say that, if duration of energization in the I_2 (or I_1)

direction is short and current is cut off before the rotor reaches θ_3 , then the rotor is moved back to the initial position θ_1 (or θ_2) by a positive (or negative) detent torque.

5 If current in the I_2 (or I_1) direction is continued to be passed for a sufficiently long time and the energization is cut off after the rotor stops at θ_2 (or θ_1) of the stopper 2 (or the stopper 1), then the rotor is maintained at the position by a negative detent torque. In
10 this state, if the current is switched to the I_1 (or I_2) direction, then the rotor overcomes the negative detent torque and generates a torque in the clockwise (or counterclockwise) direction to go back to the position of θ_1 (or θ_2) of the stopper 1 (or the stopper 2) and stops at
15 the position.

Thus, according to the present invention, each time the energizing direction of the coil is switched, the rotor carries out repetitive motion in the range defined by θ_2 and θ_1 , and the rotor can be set in a given direction by
20 making use of detent torque even when the coil is in the deenergization mode. Obviously, by continuously changing the period of time during which the coil is energized, the operation time of the rotor can be continuously changed accordingly.

25 By utilizing the advantage described above, the present invention can be applied to, for example, a camera shutter or the like to always hold the shutter closed by

the detent torque, open the shutter only for a required period of time by energizing a coil only when taking a photograph (for exposure), then close the shutter by inverse energization. Thereafter, the energization can be
5 cut off to maintain the shutter in the closed state by the detent torque. This feature is extremely convenient to achieve power saving.

Regarding the repetitive motion range, in a preferred form of the invention, an external mechanism for
10 forcibly restricting the rotation of the rotor (the mechanism is called the "stopper" in the invention) is provided. In the description given in conjunction with Fig. 4, the positions where the stoppers are set are defined as θ_1 and θ_2 . However, the positions at which the stoppers are
15 stopped may be extended to 180 degrees ($\theta_1 = 180$ degrees and $\theta_2 = 0$ degree) if there is no friction torque. In actual operation, however, there is friction torque or the like, and the friction torque cannot be overcome if a resultant torque stays small, leading to unstable operation.
20 According to experiment results, in order to secure stable operation, a limit value is $240/N$ degrees when the number of magnets for magnetic field is N . Furthermore, as shown in Fig. 5, if the detent torque is large, then a negative resultant torque range is theoretically produced as already
25 explained, and the setting range of the repetitive motion is unavoidably narrowed. Although it is desirable to provide a broader repetitive motion range, a compromise

must be made in relation to a required detent torque. To be more specific, if a larger initial torque in the deenergization mode is required, then the repetitive motion range inevitably becomes narrower. For this reason, in the invention, appropriate angles at which the stoppers are disposed range from $120/N$ to $240/N$ degrees in terms of central angle.

Fig. 6 is a perspective view of a second embodiment characterized by the magnet 30.

10 An example of a method for securing a broader repetitive motion range will be explained with reference to Fig. 6. In case of Fig. 6, N is 2. As illustrated, a central portion at the north pole in the cylindrical magnet 30 is axially cut to forcibly destroy magnetic balance
15 between the north pole and the south pole. According to experimental results, the repetitive motion range which was 60 degrees in the absence of the cut was nearly doubled but 110 degrees in the presence of the cut. The experiment results have also revealed that a cut amount denoted by
20 preferably ranges from 45 to 80 degrees, because an excessively small cut provides less imbalance effect, whereas an excessively large cut leads to a considerably reduced magnetic fluxes with consequent marked deterioration in characteristics. The cut in the north
25 pole portion shown in Fig. 6 is positioned parallel to the neutral. However, the cut may be provided at the south pole end, or the cut may be slightly inclined with respect

to the neutral in order to increase detent torque. The magnet shown in Fig. 6 is magnetically oriented in directions of D-D indicated by the arrows. However, cutting the magnet to be isotropic will also provide a similar advantage. Alternatively, the magnet may be provided with a uniform, narrow groove in an axial direction that is, for example, one to three times as long as an air gap and has a depth which is approximately equivalent to the length of the air gap. Further alternatively, a stopper (to be discussed in detail with reference to Fig. 8A) integrally formed on an end surface of a magnet for magnetic field may be provided with a groove or a cut having the same effect.

Fig. 7 is a perspective view of a third embodiment of the present invention that is characterized by a stator yoke.

Another embodiment for securing a broader repetitive motion range will be described in conjunction with Fig. 7 which is an enlarged view of the first stator yoke 2 of the first embodiment. The number N of magnetic poles of the magnet for magnetic field in the third embodiment is 2. Referring to Fig. 7, a polar tooth 25 is a polar tooth of a straight configuration that has an even wall thickness, a central angle β , and the same central angle in an axial direction. The central angle β of the polar tooth 25 must be set to an appropriate value to adequately supplement magnetic fluxes of the magnet 30 for magnetic field

(hereinafter referred to simply as "the magnet").

Experimental results have indicated that polar tooth 25 of first and second stator yokes preferably share the same configuration and the central angles θ thereof preferably range from $220/N$ to $260/N$ degrees in order to secure a wider repetitive motion range. The polar tooth 25 are not limited to the straight type shown in Figs. 1 and 7 in configuration. They may be triangular or trapezoidal. In such a case, the central angle θ means an angle of a root portion, i.e. a junction to a planar yoke. Polar teeth with tapered tips as in the case of triangular teeth, trapezoidal teeth, etc. tend to provide increased detent torque, making themselves suitable for applications where large detent torque is required.

Fig. 10 is a sectional view of a fourth embodiment characterized by a magnetic circuit.

Still another embodiment for securing a stable, broader repetitive motion range will be described in conjunction with Fig. 10. The sectional view in Fig. 10 has been taken perpendicularly to a rotary shaft 21 so as to show an air gap in a radial direction between polar tooth 25 and a magnet 30 for magnetic field. Components such as a coil, a bearing, a ring, and a planar yoke that are unnecessary for the explanation have been omitted. As illustrated in the drawing, the magnet 30 is circular, and the polar tooth 25 are composed of a uniform wall thickness. It can be seen that the air gaps in a circumferential

direction are formed such that they are narrower at central gaps G1 and gradually become wider toward end gaps G2.

With this arrangement, the phase of a stability point of detent torque agrees with that of a stability point of

5 exciting torque, permitting a stable, broader repetitive motion range to be secured. It is needless to say that this embodiment may be combined with a technique of the groove or cut, or a technique of the angle β of the polar tooth shown in Fig. 7.

10 Descriptions will now be given of an actuator in which a stopper mechanism is installed. As previously mentioned, it is preferable to accurately install a mechanism for restricting rotation somewhere in the actuator in accordance with the present invention.

15 Incorporating the stopper in the actuator permits space saving to be accomplished and also markedly improves easeness of use.

Fig. 8A is a perspective view of a bearing of a fifth embodiment that shows an example of a configuration
20 of a stopper included in an actuator, and Fig. 8B is a perspective view of a rotor of the fifth embodiment.

The illustrated embodiment functions as a stopper by a protuberance added to an end surface of the bearing and a protuberance added to an end surface of a magnet, which
25 restrict each other. First, referring to Fig. 8A, a first stopper protuberance 100 is integrally added to an end surface of a bearing 5. In Fig. 8B, a second stopper

protuberance 101 is integrally added to an end surface of a magnet 30 for magnetic field (hereinafter referred to simply as "the magnet 30"). When these two stopper protuberances are combined, as a rotor rotates in a clockwise direction (CW) indicated an arrow, the rotor 1 stops at a position where a surface 100B of the protuberance 100 of the bearing 5 comes in contact with a surface 101B of the protuberance 101 of the magnet 30. Conversely, as the rotor 1 rotates in a counterclockwise direction (CCW) indicated an arrow, the rotor 1 stops at a position where a surface 100A of the protuberance 100 of the bearing 5 comes in contact with a surface 101A of the protuberance 101 of the magnet 30. At this time, the repetitive motion range can be set as desired by means of central angles of the respective protuberances 100 and 101. In this embodiment, the protuberances functioning as the stoppers are integrally formed on the bearing 5 and the magnet 30. However, the protuberances may be constituted by adding a third part. It is needless to say that the components on which the stoppers are formed are not limited to the bearing 5 and the magnet 30. The stoppers may be formed by combining a part of the stator section of the actuator, e.g., the polar teeth 25, the flange 6 or the flange 7, the bobbin 29, the planar yoke 23, with a part of the rotor section, e.g., the sleeve 22 or the rotary shaft 21.

It has previously been mentioned that the presence

of friction torque causes inconveniences such as a narrower repetitive motion range. In order to reduce the friction torque and to obtain a broader repetitive motion range and stable operation, it is effective to avoid forming a

5 magnetic circuit by using a nonmagnetic material for the upper and lower flanges 6 and 7 on both ends of the actuator 10. This is because, if the flanges are composed of a magnetic material, then a force is generated that constantly attracts the magnet 30 toward a flange surface

10 with a smaller gap due to leakage magnetic fluxes produced at an end surface of the magnet 30. As a result, an end surface of the magnet 30 is magnetically drawn toward and comes in contact with an end surface of the bearing 5, generating frictional load during a rotational motion. The

15 attracting force is not produced if the flanges are nonmagnetic, or even if such a force is produced, it will be small enough to ignore. The effect is especially noticeable in the case of a magnet of a rare earth type (e.g. sintered Nd-Fe-B magnet). For the same reason, it is

20 desirable to use a nonmagnetic or nonferrous oil-impregnated metal for the bearing 5.

Descriptions will now be given of a relationship between an appropriate detent torque T_d and a rated torque T_{rate} .

25 As has been explained in conjunction with Figs. 3, 4, and 5, the repetitive motion range tends to be narrower as the detent torque T_d approaches the rated torque T_{rate} .

The repetitive motion range becomes narrow especially if $T_d > 3 T_{rate}/4$. Conversely, if $T_d \ll T_{rate}$, then the detent torque is too small, leading to a shortcoming in which the actuator cannot be maintained in a given direction in a deenergization mode. Therefore, to maintain the actuator in the given direction, an energization holding mode in which current is continued to flow through a coil must be implemented, which is undesirable from the standpoint of energy saving. Forcibly retaining the rotor in a certain position by using a spring would add to cost. Thus, studies on various aspects carried out for the present invention have revealed that a relationship between the detent torque T_d and the rated torque T_{rate} given below is desirable for the actuator:

$$T_{rate}/4 \leq T_d \leq 3 T_{rate}/4$$

Lastly, in the first embodiment shown in Fig. 1, the first stator yoke 2 has the polar tooth 25 and the planar yoke 23 formed into one piece, and the second stator yoke 4 also has the polar tooth 25, the planar yoke 23, and the cylindrical ring 31 formed into one piece. In the present invention, however, the major parts of the stator yokes may not be integrally formed as mentioned above.

Fig. 9 is a perspective view of a sixth embodiment showing structures of discrete stator yokes.

In the sixth embodiment, a first stator yoke 2 is composed of a planar yoke 23 (not shown) and a polar tooth 25 that are discrete, and a second stator yoke 4 (not shown,

see Fig. 1) is composed of a planar yoke 23 (not shown), a polar tooth 25, and a ring 31 (not shown) that are discrete. A bobbin 29 has two guiding grooves 200 (the one on the front side is cut and not shown) for retaining the polar tooth (of the straight shape in the drawing) 25, the two guiding grooves 200 being disposed at equidistantly in a circumferential direction. Portions of the guiding grooves 200 that come in contact with distal ends of the polar tooth 25 are provided with springy beams 201. With this arrangement, by setting the depth of the grooves 200 so that it is slightly shorter than an axial length of the polar tooth 25, a stable state of contact between the polar tooth 25 and the planar yoke 23 (not shown) can be achieved even if there are slight variations in length, thus providing a stator yoke structure that restrains deterioration in magnetic efficiency even when the polar tooth 25 and the planar yoke 23 are separated. Furthermore, guides 202 are provided on top and bottom end surfaces of the bobbin 29, so that the guides 202 fit in the planar yoke 23, thereby permitting the polar tooth 25 to be positioned. The bobbin in which the polar tooth 25 have been inserted and which has been provided with windings is inserted in the cylindrical ring 31 (not shown), then the outer peripheries of the planar yoke 23 are fitted in the inner periphery of the ring 31 at both end surfaces thereof to fix these components, thus completing an armature. The structure is especially advantageous in such a case where

the axial dimension of the polar tooth 25 need to be long or the thickness of the polar tooth 25 need to be large, since the polar tooth 25 can be used in a discrete form.

Fig. 11 is a sectional view of a seventh embodiment
5 of the present invention.

In the drawing, like reference numerals as those in Fig. 1 denote like components. The seventh embodiment employs a pair of stator yokes having planar yokes 23 and cylindrical rings 31 that are integrally formed, a lower
10 flange being made integral with the stator yokes by resin molding. With this arrangement, the number of components can be reduced, and concentricity of the stator yokes and a bearing can be improved.

Thus, according to the present invention, an
15 actuator having unique characteristics that provides large detent torque can be implemented by employing an armature that has a simple structure and an inexpensive single-phase claw pole structure. It is obvious that use of the armature having the claw pole structure that features a
20 round external configuration permits easy assembly and high magnetic efficiency.

Moreover, the actuator allows a rotor thereof to be always urged by detent torque in a given direction in a deenergization mode, thus contributing power saving. There
25 is another advantage in that the stopper mechanism is incorporated in the actuator to permit space saving.

WHAT IS CLAIMED IS:

1. A claw pole type actuator of a single-phase structure, comprising:

a stator yoke composed of a pair of substantially circular planar yokes formed of a soft magnetic material, polar teeth which axially protrude from inner peripheral edges of the respective planar yokes and which are disposed to face each other, extending in an axial direction, and a cylindrical ring provided on outer peripheral edges of one of said planar yokes;

an armature being constituted by installing a coil formed by winding a magnet wire in a coil receiving section shaped like an annular recess formed by said planar yokes, said polar teeth, and said cylindrical ring of said stator yoke; and

a stator assembly which has flanges with bearings provided on both end surfaces of said armature and in which a rotor provided with a magnet for a magnetic field composed of a permanent magnet being installed to face said polar teeth of said stator with a minute gap provided therebetween;

wherein a number of said polar teeth equals a number N of rotor magnetic poles.

2. An actuator according to Claim 1, wherein said stator yoke is comprised of a first stator yoke in which a

planar yoke and a polar tooth are combined into one piece, and a second stator yoke in which a planar yoke, a polar tooth and a cylindrical ring are combined into one piece, and said polar teeth of said first and second stator yokes, respectively, are disposed at an spacing of approximately 180 degrees in terms of an electrical angle.

3. An actuator according to Claim 1, wherein a pair of stator yokes, each being composed of said planar yoke and said cylindrical ring that are combined into one piece, are disposed to face each other.

4. An actuator according to Claim 1, wherein a rotation of said rotor is restricted by a stopper so that a maximum angle of the rotational motion stays within a range of 120/N to 240/N degrees.

5. An actuator according to Claim 4, wherein said stopper is incorporated in said actuator.

6. An actuator according to Claim 1, wherein a groove or a cut for destroying magnetic balance is provided in an axial direction on a central portion of one of south pole and north pole of said magnet for magnetic field.

7. An actuator according to Claim 1, wherein extensions of said two polar teeth in a circumferential

direction are all the same and stay within a range of 220/N to 260/N degrees at central angle.

8. An actuator according to Claim 1, wherein air gaps in a radial direction formed by said polar teeth and said rotor magnet are uneven, and air gaps at central portions of said polar teeth are narrower than air gaps at ends of said polar teeth.

9. An actuator according to Claim 1, wherein said flanges are composed of a nonmagnetic material.

10. An actuator according to Claim 1, wherein a relationship between a detent torque T_d (Nm) and a rated torque T_{rate} (Nm) is as follows:

$$T_{rate}/4 \leq T_d \leq 3 T_{rate}/4$$

where T_{rate} denotes a maximum torque value obtained when a rated current is passed, and detent torque T_d denotes a maximum torque when a coil is in a deenergization mode.

ABSTRACT OF THE DISCLOSURE

An inexpensive, small, high-efficiency actuator having a single-phase claw pole structure permits easy assembly or winding and enables a rotor to act in a fixed direction by detent torque even in a deenergization mode. The actuator includes a stator yoke composed of a pair of substantially circular toroidal planar yokes formed of a soft magnetic material, polar teeth which axially protrude from inner peripheral edges of the respective planar yokes and which are disposed so that they face each other, extending in a circumferential direction, and a stator yoke that has a cylindrical ring provided on outer peripheral edges of the planar yokes; an armature being constituted by installing a coil formed by winding a magnet wire in a coil receiving section shaped like an annular recess formed by the planar yokes, the polar teeth, and the cylindrical ring of the stator yoke; and a stator assembly which has flanges with bearings provided on both end surfaces of the armature and in which a rotor provided with a magnet for a magnetic field composed of a permanent magnet being installed such that it faces the polar teeth of the stator with minute gaps provided therebetween; wherein the number of the polar tooth equals the number N of rotor magnetic poles (N is 2 or 4).

FIG. 1

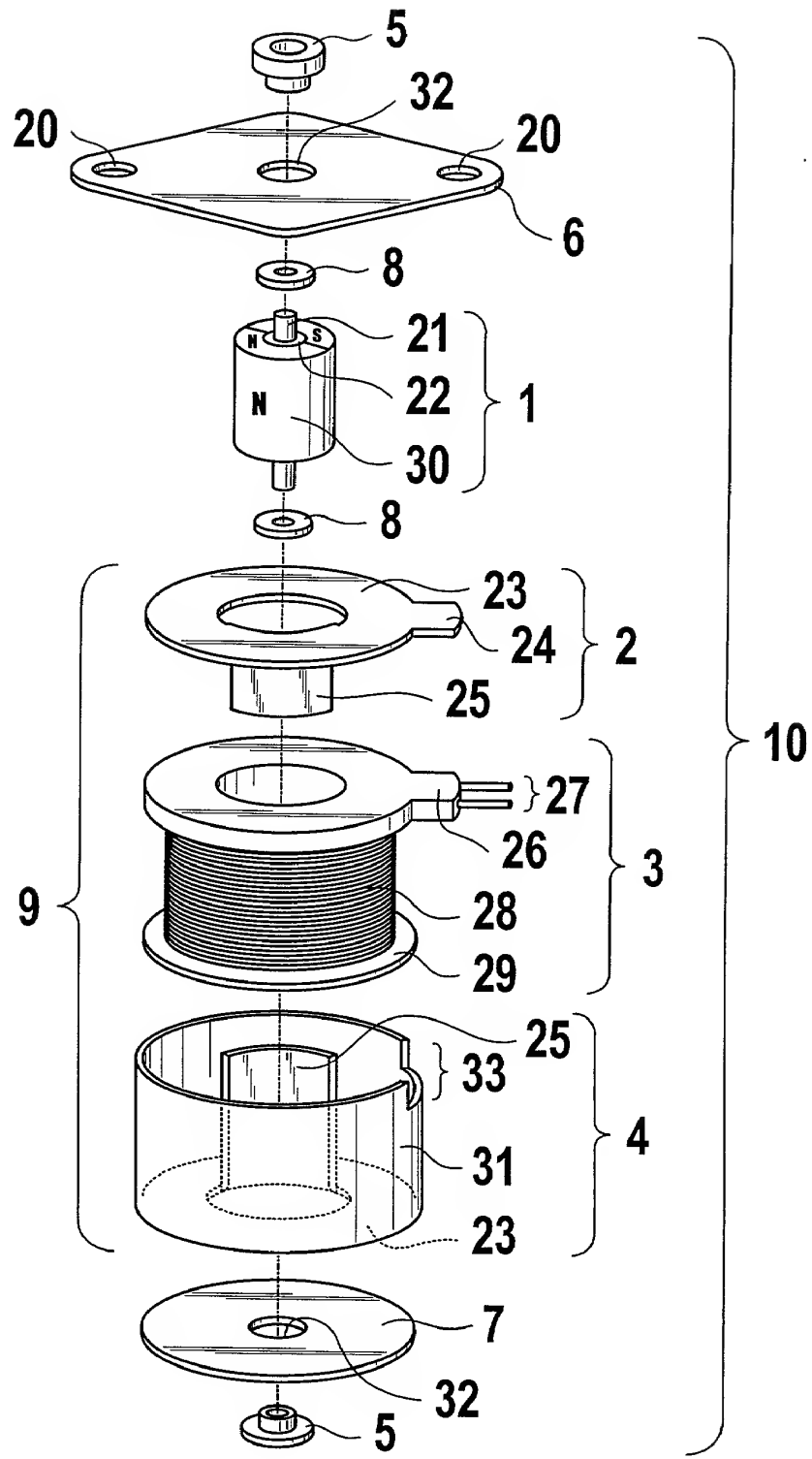


FIG. 2A

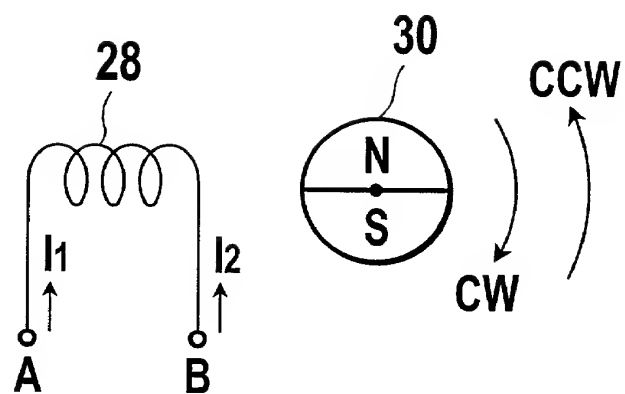


FIG. 2B

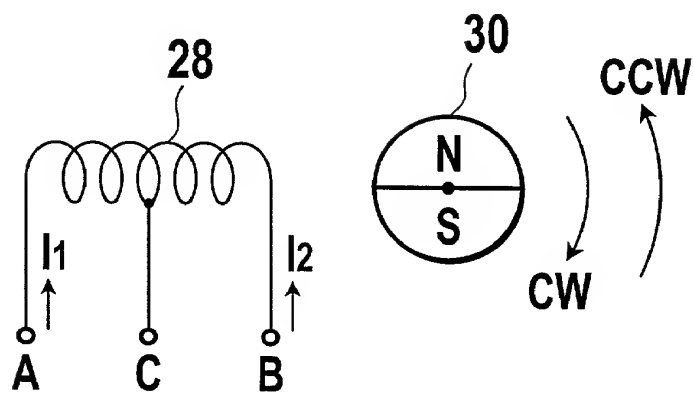


FIG. 3

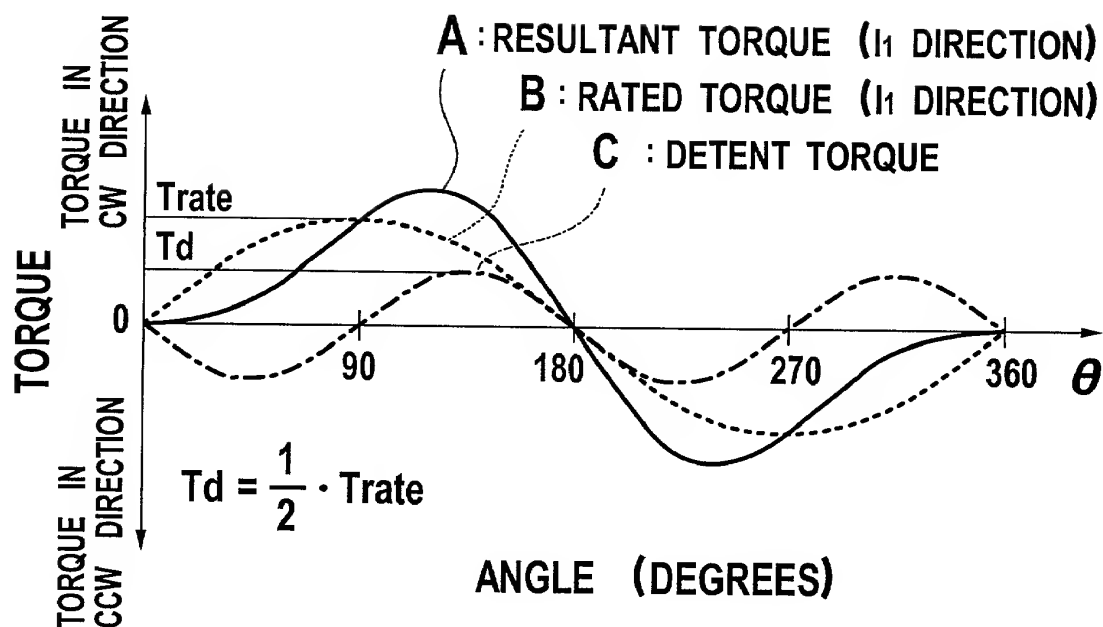


FIG. 4

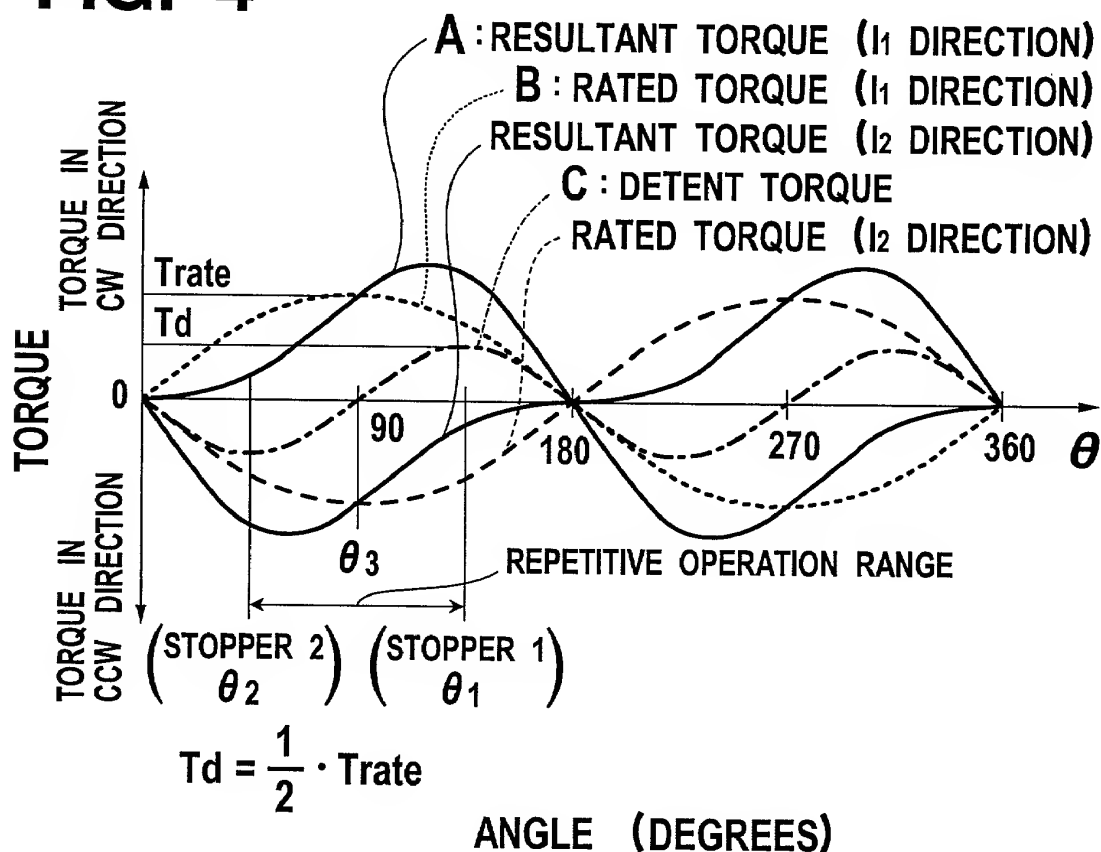


FIG. 5

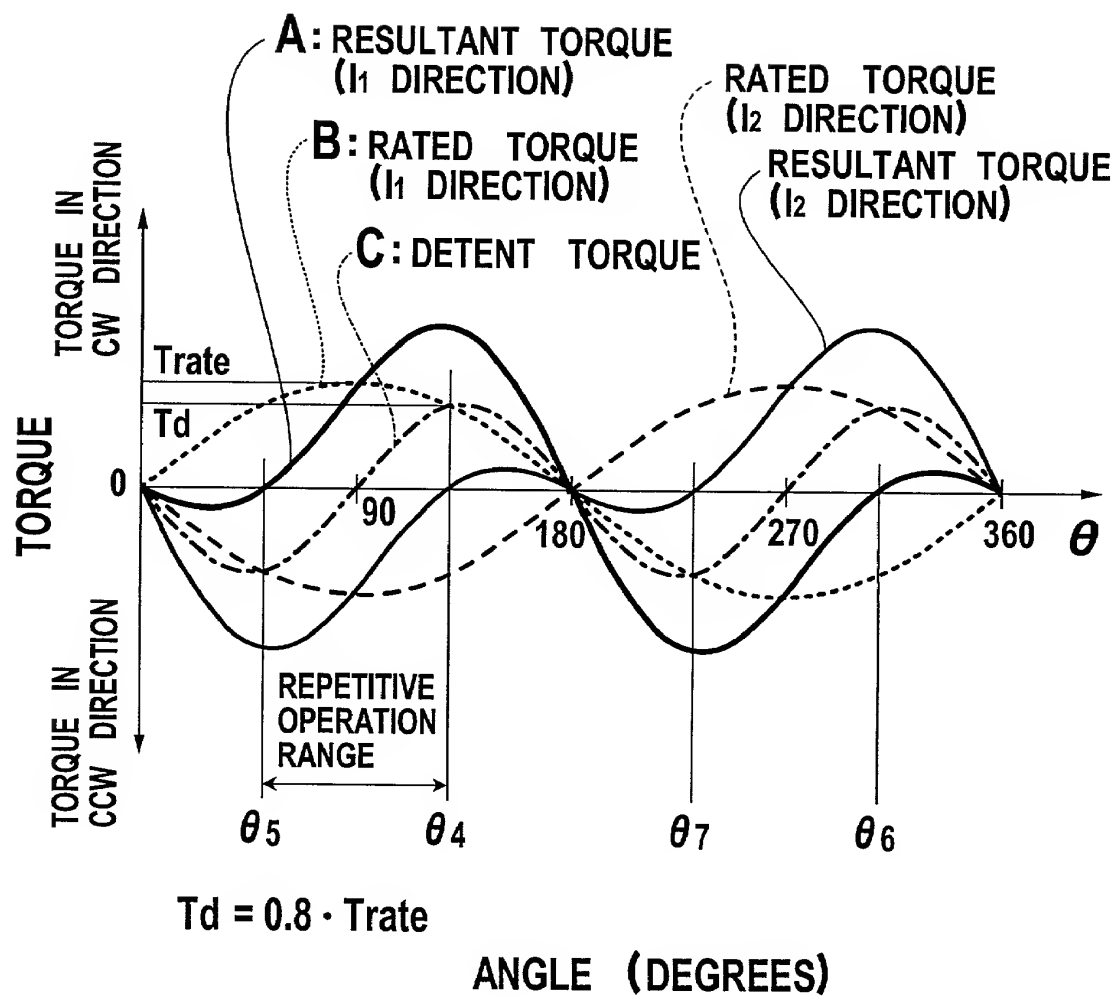


FIG. 6

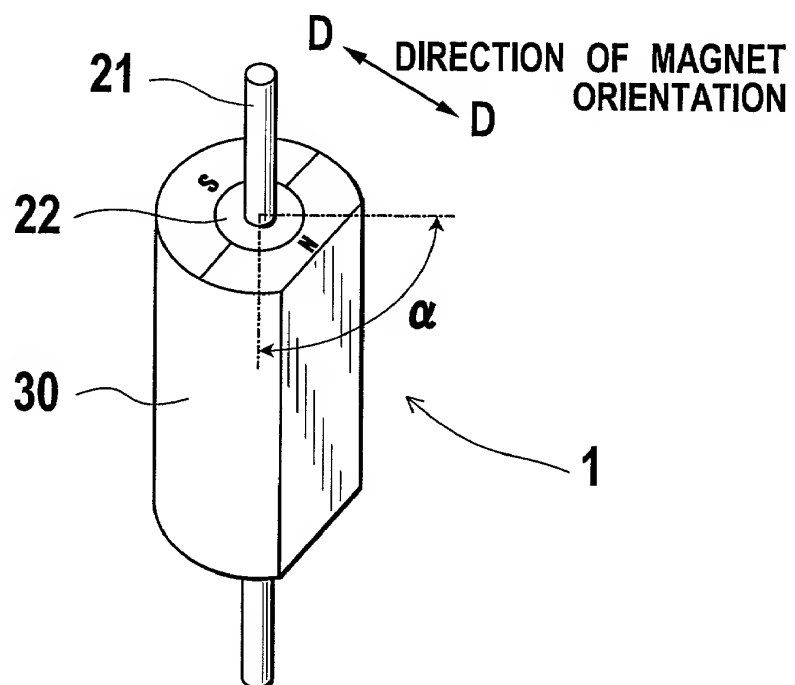


FIG. 7

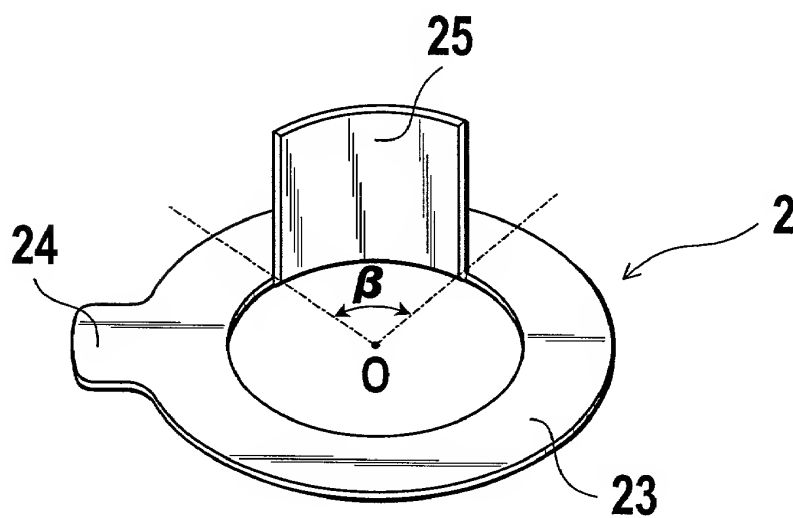


FIG. 8A

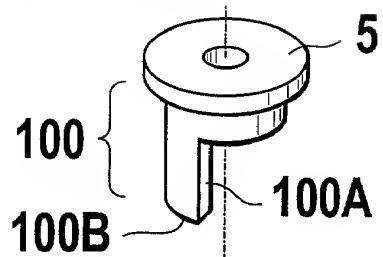


FIG. 8B

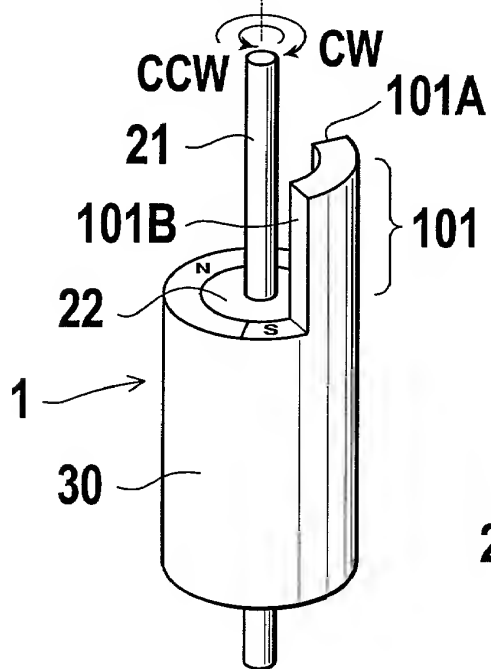


FIG. 9

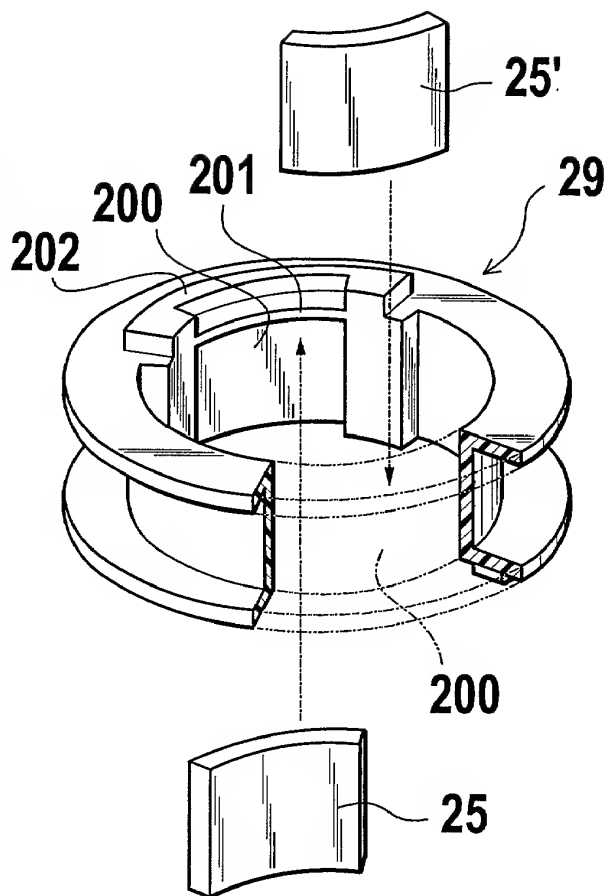


FIG. 10

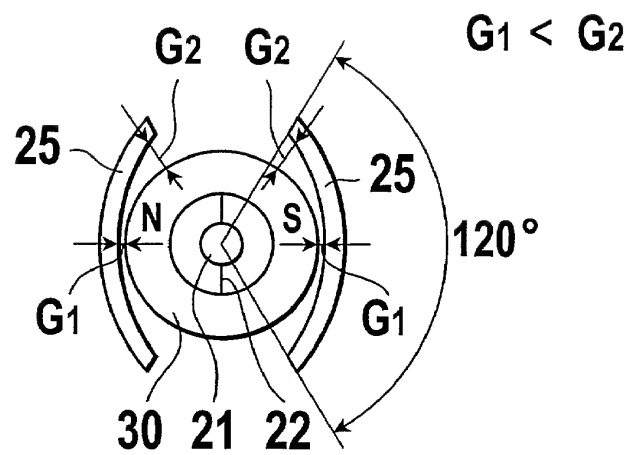
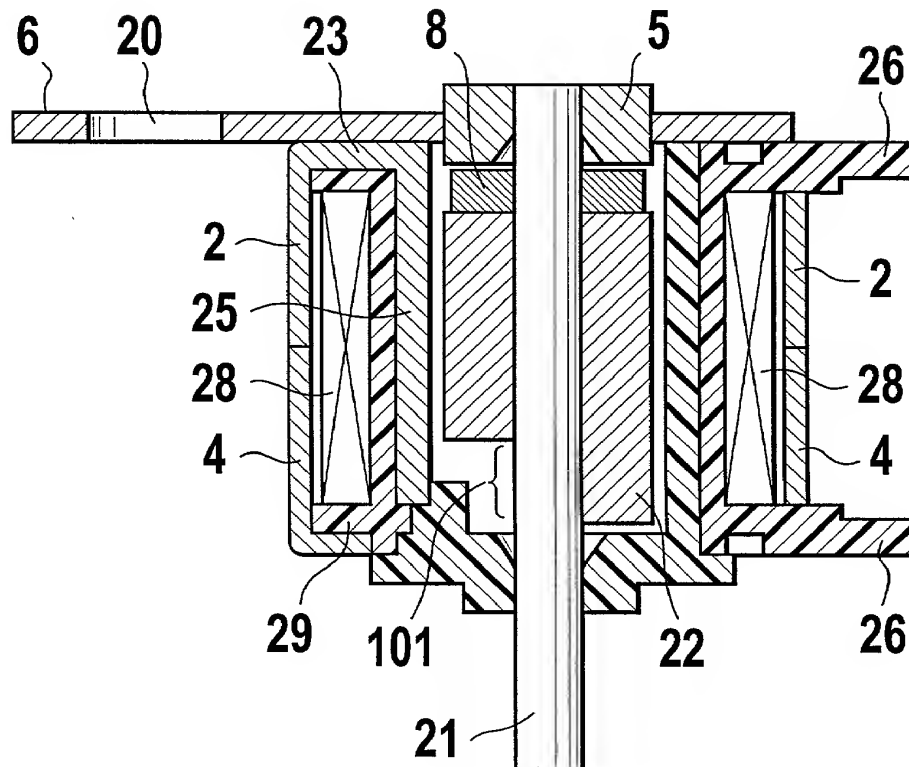


FIG. 11



COMBINED DECLARATION AND POWER OF ATTORNEY

(Original, Design, National Stage of PCT or CIP Application)

Inventors:

Yuzuru Suzuki, Sakae Fujitani and Masaki Kagawa

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are stated below next to my name, I believe I am the original, first and sole inventor (if only one name is listed above) or an original, first and joint inventor along with those listed above (if plural names are listed above) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

ACTUATOR

the specification of which: (Complete (a), (b) or (c) for type of application)

REGULAR OR DESIGN APPLICATION

- (a) x is attached hereto.
- (b) was filed on as Application Serial No. and was amended on (if applicable).

PCT FILED APPLICATION ENTERING NATIONAL STAGE

- (c) was described and claimed in International Application No. filed on and as amended on (if any).

ACKNOWLEDGEMENT OF REVIEW OF PAPERS AND DUTY OF CANDOR

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to patentability of any existing claim of this application in accordance with Title 37, Code of Federal Regulations §1.56(a).

 In compliance with this duty there is attached an information disclosure statement.
37 CFR 1.97.

PRIORITY CLAIM

I hereby claim foreign priority benefits under Title 35, United States Code, §119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed.

[Complete (d) or (e)]

(d) ☐ no such applications have been filed.

(e) ☒ such applications have been filed as follows.

EARLIEST FOREIGN APPLICATION(S), IF ANY FILED WITHIN 12 MONTHS (6 MONTHS FOR DESIGN) PRIOR TO SAID APPLICATION

Country	Application No.	Date of filing (day, month, year)	Date of issue (day, month, year)	Priority (day, month, year)	Claimed
Japan	344528/1998	3/12/1998			<input checked="" type="checkbox"/> YES NO <input type="checkbox"/>
					<input type="checkbox"/> YES NO <input type="checkbox"/>

ALL FOREIGN APPLICATION(S), IF ANY FILED MORE THAN 12 MONTHS (6 MONTHS FOR DESIGN) PRIOR TO SAID APPLICATION

CLAIM FOR BENEFIT OF PRIOR U.S. PROVISIONAL APPLICATION(S)

I hereby claim the benefit under Title 35, United States code, § 119(e) of any United States provisional application(s) listed below:

(Provisional Application Number)	(Filing Date)
(Provisional Application Number)	(Filing Date)

CONTINUATION-IN-PART

(Complete this part only if this is a continuation-in-part application)

I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, §112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, §1.56(a) which occurred between the filing date of the prior application and the national or PCT international filing date of this application.

(Application Serial No.)	(Filing Date)	(Status)	(Patent, pending, abandoned)
(Application Serial No.)	(Filing Date)	(Status)	(Patent, pending, abandoned)

POWER OF ATTORNEY

As a named inventor, I hereby appoint the following attorney and/or agent to prosecute this application and transact all business in the U.S. Patent and Trademark Office connected therewith, before all competent international authorities in connection with any international application, and before all foreign patent offices in connection with the national phase of any international application or any foreign application, and to appoint any associate attorneys in connection with any application, either domestic, international or foreign national.

John M. Howell (25,261); Richard E. Haferkamp (29,072); Kenneth Solomon (31,427); Joseph M. Rolnicki (32,653); Joseph E. Walsh, Jr. (36,959); Alan H. Norman (32,285); Donald R. Holland (35,197); Bryan K. Wheelock (31,441); Charles E. Dunlap (35,124); Anthony G. Simon (40,813); Alan L. Cassel (35,842); Michael J. Thomas (39,857); Thomas A. Polcyn (41,256); Melodie W. Henderson (37,848)

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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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